# Checking the Geometric Accuracy of a Machine Tool for Selected Geometric Parameters

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#### Abstract

This paper deals with the control parameters for selected geometric accuracy measurements for a machine tool. The parameters were needed after a refurbished milling machine was purchased. After setting up the machine, it was necessary to check the geometric accuracy that can be used for precise milling. The whole check was performed in accordance with ISO 10791. Only selected parameters of geometric accuracy were inspected, and they were later compared with the prescribed values. On the basis of a comparison of these values we were able to determine whether the machine tool can be used for accurate machining.

spindle, and deviation can be controlled thanks to the rotation of the spindle. Before making the measurements we had to remove the drag-stones, which are hindered by the measurements. Ten measurements were performed, and the values were processed.



Figure 2: Measurement scheme [1]

$$u_A = \frac{\frac{n}{i=1}(Xi - \overline{X})^2}{n \cdot (n-1)} = 8.33 \cdot 10^{-4} \,\mathrm{mm}$$
$$X = \overline{X} \pm u_A$$
$$X = (0.00750 \pm 0.00083) \,\mathrm{mm}$$

Measured value:  $(0.00750 \pm 0.00083)$  mm Value according to the standard: 0.01 mm The milling machine is satisfactory in terms of this test.

#### Test G10A

This test was conducted inside the spindle at a height of 10 mm above the drag-stones. The measurement was based on the fact that the dial indicator was attached to the internal surface of the spindle, and the deviation can be controlled thanks to the rotation of the spindle. Again, ten measurements were performed and the values were processed [3]. Finally, the drag-stones were remounted on the spindle.

$$u_A = \frac{\frac{n}{i=1}(Xi - \overline{X})^2}{n \cdot (n-1)} = 7.65 \cdot 10^{-4} \text{ mm}$$
$$X = \overline{X} \pm u_A$$
$$X = (0.00350 \pm 0.00077) \text{ mm}$$

Measured value:  $(0.00350 \pm 0.00077)$  mm Value according to the standard: 0.005 mm The milling machine is satisfactory in terms of this test.



Figure 3: Measurement scheme [1]

# Test G11A

This test was conducted at the end of the spindle. The mandrel is clamped to the spindle and the peripheral whipping was evaluated. The perpendicular axis of the mandrel (or the spindle on the axis of the longitudinal feed table) was checked before starting the measurements [3]. Thus control was important for precise testing of the peripheral spindle whipping. The measurement was based on the fact that dial indicator was attached to the mandrel.



Figure 4: Measurement scheme [1]

$$u_A = \frac{\frac{n}{i=1}(Xi - \overline{X})^2}{n \cdot (n-1)} = 8.16 \cdot 10^{-4} \text{ mm}$$
$$X = \overline{X} \pm u_A$$
$$X = (0.013\,00 \pm 0.000\,82) \text{ mm}$$

Measured value:  $(0.01300 \pm 0.00082)$  mm Value according to the standard: 0.01 mm The milling machine is unsatisfactory in terms of this test.

# Test G11B

This test was conducted at a distance of 110 mm from the end of the milling spindle. The mandrel was clamped into the milling spindle, and peripheral whipping was carried out. It was not necessary to check the perpendicularity of the axis of the mandrel because this had been done in previous measurements. The measurements were taken after measuring at a distance of 110 mm from the end of the spindle and after establishing a magnetic pedestal with a dial indicator on the milling table. The measurements were based on the fact that the mandrel was attached to the dial indicator and the deviation was controlled during rotation. For this test, it was necessary to convert the allowed values according to [1], because the tolerance on a measured length of 300 mm is given by the standard [3]. Our measurement was performed on a length of 110 mm.



Figure 5: Measurement scheme [1]

$$u_A = \frac{\prod_{i=1}^{n} (Xi - \overline{X})^2}{n \cdot (n-1)} = 8.5 \cdot 10^{-4} \text{ mm}$$
$$X = \overline{X} \pm u_A$$
$$X = (0,023\,00 \pm 0.000\,85) \text{ mm}$$

Conversion of standard values for length 110 mm: length 300 mm allows 0.01 mm according to  $[1] \Rightarrow$  allowed 1 mm on:  $0.01/300 = 3.33 \cdot 10^{-5}$  mm  $\Rightarrow$ 110 mm = 0.014 mm

Measured value:  $(0.023\,00 \pm 0.000\,85)$  mm Value according to the standard: 0.014 mm The milling machine is unsatisfactory in terms of this test.

# Test G12

This test was conducted at a distance of 110 mm. The mandrel was clamped to the milling spindle and axial parallelism was carried out with spindle movement on the Z axis. Measurements were taken after measuring a distance of 110 mm and after establishing a magnetic pedestal with a dial indicator on the milling table. Ten measurements were performed at position  $0^{\circ}$ , and the next ten measurements were performed at mandrel rotation  $180^{\circ}$ , in order to eliminate errors resulting from inaccuracies of the mandrel itself. For this test, it was necessary to convert the allowed values according to [1], because the tolerance given by the standard is for a measured length of 300 mm. Our measurement was performed on a length of 110 mm.



Figure 6: Measurement scheme [1]

$$u_A = \frac{\frac{n}{i=1}(Xi - \overline{X})^2}{n \cdot (n-1)} = 8.16 \cdot 10^{-4} \text{ mm}$$
$$X = \overline{X} \pm u_A$$
$$X = (0.003\,00 \pm 0.000\,82) \text{ mm}$$

Conversion of standard values for length 110 mm: length 300 mm allows 0.015 mm according to  $[1] \Rightarrow$  allowed 1 mm on: 0.015/300 = 5  $\cdot$  10<sup>-5</sup> mm  $\Rightarrow$ on 110 mm = 0.0055 mm

Measured value:  $(0.003 \pm 0.000 82)$  mm Value according to the standard: 0.0055 mm The milling machine is satisfactory in terms of this test.

#### Test G5A

This test was conducted at a distance of 1000 mm and was performed in the transverse direction. A coincidence spirit level was set up on the milling table, and was gradually placed at three locations. First, on the right side of the table, then in the middle, and finally on the left side. In each of these positions we gradually made ten measurements. After these measurements, the coincidence spirit level was rotated 180°, and the measurements were again performed ten times in the same places [4]. The measurements were based on the fact that the examined deviation of each of the halves inside the coincidence spirit level and the deflection were recorded at the time when the two halves for the spirit level were established [2]. The resultant values were obtained by differential measurements of the maximum and minimum values.



Figure 7: Measurement scheme [1]

$$u_{A} = (u_{AP} + u_{AL})/2$$

$$X = X_{max} - X_{min}$$

$$X = X_{P} - X_{L} = (0.1900 \pm 0.0047) \text{ mm}$$

$$u_{AP} = \frac{\frac{n}{i=1}(Xi_{P} - \overline{X}_{P})^{2}}{n \cdot (n-1)} = 4.43 \cdot 10^{-3} \text{ mm}$$

$$X_{P} = \overline{X}_{P} \pm u_{AP} = (2.1200 \pm 0.0044) \text{ mm}$$

$$u_{AS} = \frac{\frac{n}{i=1}(Xi_{S} - \overline{X}_{S})^{2}}{n \cdot (n-1)} = 0.010089 \text{ mm}$$

$$X_{S} = \overline{X}_{S} \pm u_{AS} = (2.076\,000 \pm 0.010\,089) \text{ mm}$$

$$u_{AL} = \frac{\frac{n}{i=1}(Xi_{L} - \overline{X}_{L})^{2}}{n \cdot (n-1)} = 5 \cdot 10^{-3} \text{ mm}$$

$$X_L = \overline{X}_L \pm u_{AL} = (1.930 \pm 0.005) \text{ mm}$$

Measured value:  $(0.1900 \pm 0.0047)$  mm Value according to the standard: 0.04 mm The milling machine is unsatisfactory in terms of this test.

## Test G4A

This test was conducted at a distance of 1 000 mm, and was performed in the longitudinal direction. A coincidence spirit level was set up on the milling table and was gradually placed at three locations. The order of the placements was as for the previous measurement. In each of these positions we gradually made ten measurements [3]. In essence, the principle of measurement was the same as in test G5a (above).



Figure 8: Measurement scheme [1]

$$u_{A} = (u_{AS} + u_{AP})/2$$

$$X = X_{P} - X_{L} = X_{\max} - X_{\min}$$

$$X = X_{S} - X_{P} = (0.2000 \pm 0.0095) \text{ mm}$$

$$u_{AP} = \frac{\frac{n}{i=1}(Xi_{P} - \overline{X}_{P})^{2}}{n \cdot (n-1)} = 0.011 \text{ mm}$$

$$X_{P} = \overline{X}_{P} \pm u_{AP} = (2.630 \pm 0.011) \text{ mm}$$

$$u_{AS} = \frac{\frac{n}{i=1}(Xi_{S} - \overline{X}_{S})^{2}}{n \cdot (n-1)} = 0.0079 \text{ mm}$$

$$X_{S} = \overline{X}_{S} \pm u_{AS} = (2.8300 \pm 0.0079) \text{ mm}$$

$$u_{AL} = \frac{\frac{n}{i=1}(Xi_{L} - \overline{X}_{L})^{2}}{n \cdot (n-1)} = 0.0089 \text{ mm}$$

$$X_{L} = \overline{X}_{L} \pm u_{AL} = (2.7100 \pm 0.0089) \text{ mm}$$

Measured value:  $(0.2000 \pm 0.0095)$  mm Value according to the standard: 0.06 mm The milling machine is unsatisfactory in terms of this test.

## Test 8A and test 8B

This test was conducted at a distance of 500 mm. Individual measurements were performed after 50 mm. The measurements were based on the fact that the magnetic pedestal was attached to the structure of the mill. The point of the dial indicator was attached to the surface side of the guide groove. The measured deflection was noted every 50 mm with the passing of the groove [5]. Then we measured the opposite side of the guide groove. The principle is exactly the same as in test 8a (above).



Figure 9: Measurement scheme [1]

$$u_{A} = \frac{\frac{n}{i=1}(Xi - \overline{X})^{2}}{n \cdot (n-1)} = 4.69 \cdot 10^{-3} \text{ mm}$$

$$X = \overline{X} \pm u_{A} = (0.0230 \pm 0.0047) \text{ mm}$$

$$u_{A} = \frac{\frac{n}{i=1}(Xi - \overline{X})^{2}}{n \cdot (n-1)} = 1.95 \cdot 10^{-3} \text{ mm}$$

$$X = \overline{X} \pm u_{A} = (0.0073 \pm 0.0020) \text{ mm}$$

**Measured value:**  $(0.0230 \pm 0.0047)$  mm

Value according to the standard: 0.02 mm The milling machine is **unsatisfactory** in terms of this test. (8a test)

**Measured value:**  $(0.0073 \pm 0.0020)$  mm

Value according to the standard: 0.02 mm The milling machine is **satisfactory** in terms of this test. (8b test)

# Test G17

This test was conducted on the right and left side of the milling table. First, a ruler had to be assembled at a distance of 250 mm from the centre of the table to the right side and then on the left side of the milling table. Ten measurements were performed for the right side, and then ten measurements for the left side.



Figure 10: Measurement scheme [1]

$$u_{AP} = \frac{\overline{(Xi_P - \overline{X}_P)^2}}{n \cdot (n-1)} = 1.25 \cdot 10^{-3} \text{ mm}$$
$$u_{AL} = \frac{\overline{(Xi_L - \overline{X}_L)^2}}{n \cdot (n-1)} = 8.16 \cdot 10^{-4} \text{ mm}$$
$$X_P = \overline{X}_P \pm u_{AP} = (0.0140 \pm 0.0013) \text{ mm}$$
$$X_L = \overline{X}_L \pm u_{AL} = (0.008\ 00 \pm 0.000\ 82) \text{ mm}$$

Measured value:  $(0.0140 \pm 0.0013)$  mm Value according to the standard: 0.02 mm Measured value:  $(0.00800 \pm 0.00082)$  mm Value according to the standard: 0.02 mm The milling machine is satisfactory in terms of these tests.

# Conclusions

This paper has reported on tests of selected geometrical precision parameters for a milling machine in the laboratories of the Department of Machining and Assembly, Faculty of Mechanical Engineering,  $V\check{S}B$  – Technical University of Ostrava. The measurements were performed after selecting suitable tests and providing the necessary gauges and equipment for the tests.

On the basis of the results of the geometric precision tests for a milling machine with a vertical spindle, the following conclusions can be drawn:

- The milling machine failed 5 out of the 10 tests that were performed.
- Measurement of the middle guide groove, parallel to table feed at a distance of 500 mm (test 8a): the main reason for the unsatisfactory test results was the groove that ran through the whole side. The same measurement was therefore performed on the opposite side of the groove, and in this case c ompliance was achieved.
- Measurement of the angular deviation movement on the Y axis (test G5a), and measurement of the angular deviation movement on the X axis (test G4a): the main reason for the unsatisfactory test result was bad setting up in the laboratory. It was not possible to establish into the correct position, because the milling machine was not equipped with establishing screws.
- The peripheral whipping measurement the internal taper spindle at the end of the spindle (test G11a) and the peripheral whipping measurement – the internal taper spindle at a distance of 110 mm from the end of the spindle (test G11b): the main reason for the unsatisfactory test result was perhaps gear-wear with a constant gear ratio inside the milling head, or bearing-wear. In order to eliminate this inac-

curacy, it would be necessary to overhaul the milling head.

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## References

 ISO 10791-2 – Test conditions for machine centres — Part 2: Geometric tests for machines with vertical spindle or universal heads with vertical primary rotary axis (vertical Z-axis).

- [2] Tichá, Š.: Strojírenská metrologie část 1. Ostrava : VŠB TU Ostrava, 2006, p. 112. ISBN 80-248-0671-1.
- [3] Brázda, F.: Kontrola vybraných parametrů geometrické přesnosti obráběcího stroje. Ostrava : Katedra obrábění a montáže, 2006. Bakalářská práce. VŠB – Technical University of Ostrava. Bachelor project supervisor: Robert Čep.
- [4] Čep, R., Janásek, A., Valíček, J., Čepová, L.: Testing of Greenleaf Ceramic Cutting Tools with and Interrupted Cutting. *Tehnički Vjestnik – Technical Gazette.* Vol. **18**, no. 3, 2011, p. 327–332. ISSN 1330-3651.
- [5] ISO 10791-1 Test conditions for machine centres — Part 1: Geometric tests for machines with horizontal spindle and with accessory heads (horizontal Z-axis).